## FEATURES

High speed<br>$400 \mathrm{MHz},-3 \mathrm{~dB}$ full power bandwidth<br>2000 V/ $\mu \mathrm{s}$ slew rate<br>Fixed gain of 2 with no external components<br>Internal common-mode feedback to improve gain and phase balance: - $\mathbf{6 0} \mathbf{~ d B}$ @ 10 MHz<br>Separate input to set the common-mode output voltage<br>Low distortion: 68 dB SFDR @ 5 MHz $200 \Omega$ load<br>Power supply range +2.7 V to $\pm 5 \mathrm{~V}$

## APPLICATIONS

## Video line driver

Digital line driver
Low power differential ADC driver
Differential in/out level shifting
Single-ended input to differential output driver

## GENERAL DESCRIPTION

The AD8131 is a differential or single-ended input to differential output driver requiring no external components for a fixed gain of 2. The AD8131 is a major advancement over op amps for driving signals over long lines or for driving differential input ADCs. The AD8131 has a unique internal feedback feature that provides output gain and phase matching that are balanced to -60 dB at 10 MHz , reducing radiated EMI and suppressing harmonics. Manufactured on the Analog Devices, Inc. next generation XFCB bipolar process, the AD8131 has a -3 dB bandwidth of 400 MHz and delivers a differential signal with very low harmonic distortion.

The AD8131 is a differential driver for the transmission of high-speed signals over low-cost twisted pair or coax cables. The AD8131 can be used for either analog or digital video signals or for other high-speed data transmission. The AD8131 driver is capable of driving either Cat 3 or Cat 5 twisted pair or coax with minimal line attenuation. The AD8131 has considerable cost and performance improvements over discrete line driver solutions.

The AD8131 can replace transformers in a variety of applications, preserving low frequency and dc information. The AD8131 does not have the susceptibility to magnetic interference and hysteresis of transformers. It is smaller, easier to work with, and has the high reliability associated with ICs.

## Rev. B

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## FUNCTIONAL BLOCK DIAGRAM



Figure 1.


Figure 2. Output Balance Error vs. Frequency
The AD8131's differential output also helps balance the input for differential ADCs, optimizing the distortion performance of the ADCs. The common-mode level of the differential output is adjustable by a voltage on the Vосм pin, easily level-shifting the input signals for driving single-supply ADCs with dual supply signals. Fast overload recovery preserves sampling accuracy.

The AD8131 is available in both SOIC and MSOP packages for operation over $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.

[^0]
## AD8131

## TABLE OF CONTENTS

Specifications .....  3
$\pm \mathrm{D}_{\text {IN }}$ to $\pm$ OUT Specifications ..... 3
V осм to $\pm$ OUT Specifications .....  4
$\pm \mathrm{D}_{\text {IN }}$ to $\pm$ OUT Specifications. .....  5
$V_{\text {OCM }}$ to $\pm$ OUT Specifications .....  6
Absolute Maximum Ratings .....  7
ESD Caution ..... 7
Pin Configuration and Function Descriptions. .....  8
Typical Performance Characteristics .....  9
Operational Description ..... 15
Theory of Operation ..... 16
Analyzing an Application Circuit. ..... 16
Closed-Loop Gain ..... 16

## REVISION HISTORY

6/05-Rev. A to Rev. BUpdated Format.Changed Upper Operating Limit ..... UniversalUniversal
Changes to Ordering Guide ..... 20
Estimating the Output Noise Voltage ..... 16
Calculating the Input Impedance of an Application Circuit. ..... 16
Input Common-Mode Voltage Range in Single-Supply Applications ..... 17
Setting the Output Common-Mode Voltage ..... 17
Driving a Capacitive Load. ..... 17
Applications ..... 18
Twisted-Pair Line Driver ..... 18
3 V Supply Differential A-to-D Driver ..... 18
Unity-Gain, Single-Ended-to-Differential Driver ..... 19
Outline Dimensions ..... 20
Ordering Guide ..... 20

## SPECIFICATIONS

## $\pm \mathrm{D}_{\text {IN }}$ TO $\pm$ OUT SPECIFICATIONS

$25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{s}}= \pm 5 \mathrm{~V}, \mathrm{~V}_{\text {ocm }}=0 \mathrm{~V}, \mathrm{G}=2, \mathrm{R}_{\mathrm{L}, \mathrm{dm}}=200 \Omega$, unless otherwise noted. Refer to Figure 5 and Figure 39 for test setup and label descriptions. All specifications refer to single-ended input and differential outputs, unless otherwise noted.

Table 1.

\begin{tabular}{|c|c|c|c|c|c|}
\hline Parameter \& Conditions \& Min \& Typ \& Max \& Unit \\
\hline \begin{tabular}{l}
DYNAMIC PERFORMANCE \\
-3 dB Large Signal Bandwidth -3 dB Small Signal Bandwidth Bandwidth for 0.1 dB Flatness Slew Rate Settling Time Overdrive Recovery Time
\end{tabular} \& \[
\begin{aligned}
\& \mathrm{V}_{\text {OUT }}=2 \mathrm{~V} \text { p-p } \\
\& \mathrm{V}_{\text {out }}=0.2 \mathrm{~V} \text { p-p } \\
\& \mathrm{V}_{\text {out }}=0.2 \mathrm{~V} \text { p-p } \\
\& \mathrm{V}_{\text {OUT }}=2 \mathrm{~V} \text { p-p, } 10 \% \text { to } 90 \% \\
\& 0.1 \%, \mathrm{~V}_{\text {OUT }}=2 \mathrm{~V} \text { p-p } \\
\& \mathrm{V}_{\text {IN }}=5 \mathrm{~V} \text { to } 0 \mathrm{~V} \text { Step }
\end{aligned}
\] \& \& \[
\begin{aligned}
\& 400 \\
\& 320 \\
\& 85 \\
\& 2000 \\
\& 14 \\
\& 5 \\
\& \hline
\end{aligned}
\] \& \& \begin{tabular}{l}
MHz \\
MHz \\
MHz \\
V/ \(\mu \mathrm{s}\) \\
ns \\
ns
\end{tabular} \\
\hline \begin{tabular}{l}
NOISE/HARMONIC PERFORMANCE \\
Second Harmonic \\
Third Harmonic \\
IMD \\
IP3 \\
Voltage Noise (RTO) \\
Differential Gain Error \\
Differential Phase Error
\end{tabular} \&  \& \& \[
\begin{aligned}
\& -68 \\
\& -63 \\
\& -95 \\
\& -79 \\
\& -94 \\
\& -70 \\
\& -101 \\
\& -77 \\
\& -54 \\
\& 30 \\
\& 25 \\
\& 0.01 \\
\& 0.06
\end{aligned}
\] \& \& \begin{tabular}{l}
dBc \\
dBc \\
dBc \\
dBc \\
dBc \\
dBc \\
dBC \\
dBc \\
dBc \\
dBm \\
\(\mathrm{nV} / \sqrt{ } \mathrm{Hz}\) \\
\% \\
degrees
\end{tabular} \\
\hline INPUT CHARACTERISTICS Input Resistance Input Capacitance Input Common-Mode Voltage CMRR \& \begin{tabular}{l}
Single-ended input Differential input \\
\(\Delta \mathrm{V}_{\text {out }, \mathrm{dm}} / \Delta \mathrm{V}_{\mathrm{IN}, \mathrm{cm}} ; \Delta \mathrm{V}_{\mathrm{IN}, \mathrm{cm}}= \pm 0.5 \mathrm{~V}\)
\end{tabular} \& \& \[
\begin{aligned}
\& 1.125 \\
\& 1.5 \\
\& 1 \\
\& -7.0 \text { to }+5.0 \\
\& -70 \\
\& \hline
\end{aligned}
\] \& \& \[
\begin{aligned}
\& \mathrm{k} \Omega \\
\& \mathrm{k} \Omega \\
\& \mathrm{pF} \\
\& \mathrm{~V} \\
\& \mathrm{~dB}
\end{aligned}
\] \\
\hline \begin{tabular}{l}
OUTPUT CHARACTERISTICS Offset Voltage (RTO) \\
Output Voltage Swing Linear Output Current Gain Output Balance Error
\end{tabular} \& \begin{tabular}{l}
\(\mathrm{V}_{\mathrm{OS}, \mathrm{dm}}=\mathrm{V}_{\mathrm{OUT}, \mathrm{dm} ;} \mathrm{V}_{\mathrm{DIN}+}=\mathrm{V}_{\mathrm{DIN}}=\mathrm{V}_{\mathrm{OCM}}=0 \mathrm{~V}\) \\
\(\mathrm{T}_{\text {min }}\) to \(\mathrm{T}_{\text {max }}\) variation \\
Vосм \(=\) float \\
\(\mathrm{T}_{\text {min }}\) to \(\mathrm{T}_{\text {max }}\) variation \\
Maximum \(\Delta V_{\text {out; }}\) single-ended output \\
\(\Delta \mathrm{V}_{\text {out }, \mathrm{dm}} / \Delta \mathrm{V}_{\mathrm{IN}, \mathrm{dm}} ; \Delta \mathrm{V}_{\mathrm{IN}, \mathrm{dm}}= \pm 0.5 \mathrm{~V}\) \\
\(\Delta V_{\text {OUT, }} / \Delta \mathrm{V}_{\text {OUT, }} \mathrm{dm} ; \Delta \mathrm{V}_{\text {OUT, }} \mathrm{dm}=1 \mathrm{~V}\)
\end{tabular} \& 1.97 \& \[
\begin{aligned}
\& \pm 2 \\
\& \pm 8 \\
\& \pm 4 \\
\& \pm 10 \\
\& -3.6 \text { to }+3.6 \\
\& 60 \\
\& 2 \\
\& -70 \\
\& \hline
\end{aligned}
\] \& \(\pm 7\)

2.03 \& | mV |
| :--- |
| $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| mV |
| $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| V |
| mA |
| V/V |
| dB | <br>

\hline
\end{tabular}

## AD8131

## $\mathbf{V}_{\text {OCM }} \mathbf{T O} \pm$ OUT SPECIFICATIONS

$25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{s}}= \pm 5 \mathrm{~V}, \mathrm{~V}_{\text {ocm }}=0 \mathrm{~V}, \mathrm{G}=2, \mathrm{R}_{\mathrm{L}, \mathrm{dm}}=200 \Omega$, unless otherwise noted. Refer to Figure 5 and Figure 39 for test setup and label descriptions. All specifications refer to single-ended input and differential outputs, unless otherwise noted.
Table 2.

| Parameter | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DYNAMIC PERFORMANCE -3 dB Bandwidth Slew Rate | $\begin{aligned} & \Delta \mathrm{V}_{\text {осм }}=600 \mathrm{mV} \\ & \mathrm{~V} \text { осм }=-1 \mathrm{~V} \text { to }+1 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 210 \\ & 500 \end{aligned}$ |  | MHz <br> V/ $\mu \mathrm{s}$ |
| DC PERFORMANCE <br> Input Voltage Range Input Resistance Input Offset Voltage <br> Input Bias Current VOCM CMRR Gain | $\begin{aligned} & \mathrm{V}_{\mathrm{OS}, \mathrm{~cm}}=\mathrm{V}_{\mathrm{oUT}, \mathrm{~cm} ;} ; \mathrm{V}_{\mathrm{DIN}+}=\mathrm{V}_{\mathrm{DIN}-}=\mathrm{V}_{\mathrm{OCM}}=0 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{OCM}}=\text { float } \\ & \Delta \mathrm{V}_{\mathrm{OUT}, \mathrm{dm}} / \Delta \mathrm{V}_{\mathrm{OCM}} ; \Delta \mathrm{V}_{\mathrm{OCM}}= \pm 0.5 \mathrm{~V} \\ & \Delta \mathrm{~V}_{\mathrm{OUT}, \mathrm{~cm}} / \Delta \mathrm{V}_{\mathrm{OCM}} ; \Delta \mathrm{V}_{\mathrm{OCM}}= \pm 1 \mathrm{~V} \end{aligned}$ | 0.988 | $\begin{aligned} & \pm 3.6 \\ & 120 \\ & \pm 1.5 \\ & \pm 2.5 \\ & 0.5 \\ & -60 \\ & 1 \end{aligned}$ | $\pm 7$ $1.012$ | V <br> $\mathrm{k} \Omega$ <br> mV <br> mV <br> $\mu \mathrm{A}$ <br> dB <br> V/V |
| POWER SUPPLY <br> Operating Range <br> Quiescent Current <br> Power Supply Rejection Ratio | $\mathrm{V}_{\mathrm{DIN}+}=\mathrm{V}_{\mathrm{DIN}-}=\mathrm{V}_{\mathrm{OCM}}=0 \mathrm{~V}$ <br> $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ variation <br> $\Delta \mathrm{V}_{\text {out, } \mathrm{dm}} / \Delta \mathrm{V}_{\mathrm{s}} ; \Delta \mathrm{V}_{\mathrm{s}}= \pm 1 \mathrm{~V}$ | $\begin{gathered} \pm 1.4 \\ 10.5 \end{gathered}$ | $\begin{aligned} & 11.5 \\ & 25 \\ & -70 \end{aligned}$ | $\begin{gathered} \pm 5.5 \\ 12.5 \\ -56 \end{gathered}$ | V <br> mA <br> $\mu \mathrm{A} /{ }^{\circ} \mathrm{C}$ <br> dB |
| OPERATING TEMPERATURE RANGE |  | -40 |  | +125 | ${ }^{\circ} \mathrm{C}$ |

## $\pm \mathrm{D}_{\text {IN }}$ TO $\pm$ OUT SPECIFICATIONS

$25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{s}}=5 \mathrm{~V}, \mathrm{~V}_{\text {осм }}=2.5 \mathrm{~V}, \mathrm{G}=2, \mathrm{R}_{\mathrm{L}, \mathrm{dm}}=200 \Omega$, unless otherwise noted. Refer to Figure 5 and Figure 39 for test setup and label descriptions. All specifications refer to single-ended input and differential outputs, unless otherwise noted.
Table 3.

\begin{tabular}{|c|c|c|c|c|c|}
\hline Parameter \& Conditions \& Min \& Typ \& Max \& Unit \\
\hline \begin{tabular}{l}
DYNAMIC PERFORMANCE \\
-3 dB Large Signal Bandwidth \\
-3 dB Small Signal Bandwidth \\
Bandwidth for 0.1 dB Flatness \\
Slew Rate \\
Settling Time \\
Overdrive Recovery Time
\end{tabular} \& \[
\begin{aligned}
\& \text { Vout }=2 \mathrm{~V} \text { p-p } \\
\& \text { Vout }=0.2 \mathrm{~V} \text { p-p } \\
\& \mathrm{V}_{\text {out }}=0.2 \mathrm{~V} \text { p-p } \\
\& \text { Vout }=2 \mathrm{~V} \text { p-p, } 10 \% \text { to } 90 \% \\
\& 0.1 \%, \mathrm{~V}_{\text {out }}=2 \mathrm{~V} \text { p-p } \\
\& \mathrm{V}_{\text {IN }}=5 \mathrm{~V} \text { to } 0 \mathrm{~V} \text { Step }
\end{aligned}
\] \& \& \[
\begin{aligned}
\& 385 \\
\& 285 \\
\& 65 \\
\& 1600 \\
\& 18 \\
\& 5 \\
\& \hline
\end{aligned}
\] \& \& \begin{tabular}{l}
MHz \\
MHz \\
MHz \\
V/ \(\mu \mathrm{s}\) \\
ns \\
ns
\end{tabular} \\
\hline \begin{tabular}{l}
NOISE/HARMONIC PERFORMANCE \\
Second Harmonic \\
Third Harmonic \\
IMD \\
IP3 \\
Voltage Noise (RTO) \\
Differential Gain Error \\
Differential Phase Error
\end{tabular} \&  \& \& \[
\begin{aligned}
\& -67 \\
\& -56 \\
\& -94 \\
\& -77 \\
\& -74 \\
\& -67 \\
\& -95 \\
\& -74 \\
\& -51 \\
\& 29 \\
\& 25 \\
\& 0.02 \\
\& 0.08
\end{aligned}
\] \& \& \begin{tabular}{l}
dBc \\
dBc \\
dBc \\
dBc \\
dBc \\
dBc \\
dBc \\
dBc \\
dBc \\
dBm \\
\(\mathrm{nV} / \sqrt{ } \mathrm{Hz}\) \\
\% \\
degrees
\end{tabular} \\
\hline INPUT CHARACTERISTICS Input Resistance Input Capacitance Input Common-Mode Voltage CMRR \& \begin{tabular}{l}
Single-ended input \\
Differential input \\
\(\Delta \mathrm{V}_{\text {out }, \mathrm{dm}} / \Delta \mathrm{V}_{\mathrm{IN}, \mathrm{cm} ;} \Delta \mathrm{V}_{\mathrm{IN}, \mathrm{cm}}= \pm 0.5 \mathrm{~V}\)
\end{tabular} \& \& \[
\begin{aligned}
\& 1.125 \\
\& 1.5 \\
\& 1 \\
\& -1.0 \text { to }+4.0 \\
\& -70
\end{aligned}
\] \& \& \[
\begin{aligned}
\& \mathrm{k} \Omega \\
\& \mathrm{k} \Omega \\
\& \mathrm{pF} \\
\& \mathrm{~V} \\
\& \mathrm{~dB}
\end{aligned}
\] \\
\hline \begin{tabular}{l}
OUTPUT CHARACTERISTICS Offset Voltage (RTO) \\
Output Voltage Swing Linear Output Current Gain Output Balance Error
\end{tabular} \& \begin{tabular}{l}
\(\mathrm{V}_{\text {os, }} \mathrm{dm}=\mathrm{V}_{\text {out, } \mathrm{dm} ;} \mathrm{V}_{\mathrm{DIN}+}=\mathrm{V}_{\mathrm{DIN}}=\mathrm{V}_{\text {ocm }}=2.5 \mathrm{~V}\) \\
\(\mathrm{T}_{\text {min }}\) to \(\mathrm{T}_{\text {max }}\) variation \\
Vocm \(=\) float \\
\(\mathrm{T}_{\text {min }}\) to \(\mathrm{T}_{\text {max }}\) variation \\
Maximum \(\Delta V_{\text {out; }}\) single-ended output \\
\(\Delta \mathrm{V}_{\text {out }, \mathrm{dm}} / \Delta \mathrm{V}_{\mathrm{IN}, \mathrm{dm}} ; \Delta \mathrm{V}_{\mathrm{IN}, \mathrm{dm}}= \pm 0.5 \mathrm{~V}\) \\
\(\Delta \mathrm{V}_{\text {out }, \mathrm{cm}} / \Delta \mathrm{V}_{\text {OUT, }} \mathrm{dm} ; \Delta \mathrm{V}_{\text {OUT, }} \mathrm{dm}=1 \mathrm{~V}\)
\end{tabular} \& 1.96 \& \[
\begin{aligned}
\& \pm 3 \\
\& \pm 8 \\
\& \pm 4 \\
\& \pm 10 \\
\& 1.0 \text { to } 3.7 \\
\& 45 \\
\& 2 \\
\& -62
\end{aligned}
\] \& \(\pm 7\)

2.04 \& | mV |
| :--- |
| $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| mV |
| $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| V |
| mA |
| V/V |
| dB | <br>

\hline
\end{tabular}

## AD8131

## $\mathbf{V}_{\text {OCM }} \mathbf{T O} \pm$ OUT SPECIFICATIONS

$25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{s}}=5 \mathrm{~V}, \mathrm{Vocm}^{2}=2.5 \mathrm{~V}, \mathrm{G}=2, \mathrm{R}_{\mathrm{L}, \mathrm{dm}}=200 \Omega$, unless otherwise noted. Refer to Figure 5 and Figure 39 for test setup and label descriptions. All specifications refer to single-ended input and differential outputs, unless otherwise noted.
Table 4.

| Parameter | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DYNAMIC PERFORMANCE -3 dB Bandwidth Slew Rate | $\begin{aligned} & \Delta \mathrm{V} \text { осм }=600 \mathrm{mV} \\ & \mathrm{~V} \text { осм }=1.5 \mathrm{~V} \text { to } 3.5 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 200 \\ & 450 \end{aligned}$ |  | $\begin{aligned} & \mathrm{MHz} \\ & \mathrm{~V} / \mu \mathrm{s} \\ & \hline \end{aligned}$ |
| DC PERFORMANCE Input Voltage Range Input Resistance Input Offset Voltage <br> Input Bias Current Vocm CMRR Gain | $\begin{aligned} & \mathrm{V}_{\mathrm{OS}, \mathrm{~cm}}=\mathrm{V}_{\mathrm{OUT}, \mathrm{~cm} ;} \mathrm{V}_{\mathrm{DIN}+}=\mathrm{V}_{\mathrm{DIN}-}=\mathrm{V}_{\mathrm{OCM}}=2.5 \mathrm{~V} \\ & \mathrm{~V}_{\text {OCM }}=\text { float } \end{aligned}$ <br>  <br> $\Delta \mathrm{V}_{\text {out, }} \mathrm{cm} / \Delta \mathrm{V}_{\text {ocm }} ; \Delta \mathrm{V}_{\text {ocm }}=2.5 \mathrm{~V} \pm 1 \mathrm{~V}$ | 0.985 | $\begin{aligned} & 1.0 \text { to } 3.7 \\ & 30 \\ & \pm 5 \\ & \pm 10 \\ & 0.5 \\ & -60 \\ & 1 \end{aligned}$ | $\pm 12$ $1.015$ | V <br> k $\Omega$ <br> mV <br> mV <br> $\mu \mathrm{A}$ <br> dB <br> V/V |
| POWER SUPPLY <br> Operating Range <br> Quiescent Current <br> Power Supply Rejection Ratio | $\mathrm{V}_{\mathrm{DIN}+}=\mathrm{V}_{\mathrm{DIN}}=\mathrm{V}_{\text {OCM }}=2.5 \mathrm{~V}$ <br> $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ variation <br> $\Delta \mathrm{V}_{\text {out, }} \mathrm{dm} / \Delta \mathrm{V}_{\mathrm{s}} ; \Delta \mathrm{V}_{\mathrm{s}}= \pm 0.5 \mathrm{~V}$ | $\begin{aligned} & 2.7 \\ & 9.25 \end{aligned}$ | $\begin{aligned} & 10.25 \\ & 20 \\ & -70 \\ & \hline \end{aligned}$ | $\begin{aligned} & 11 \\ & 11.25 \\ & -56 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~mA} \\ & \mu \mathrm{~A} /{ }^{\circ} \mathrm{C} \\ & \mathrm{~dB} \end{aligned}$ |
| OPERATING TEMPERATURE RANGE |  | -40 |  | +125 | ${ }^{\circ} \mathrm{C}$ |

## ABSOLUTE MAXIMUM RATINGS

Table 5. ${ }^{1}$

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | $\pm 5.5 \mathrm{~V}$ |
| Vocm | $\pm \mathrm{V}_{\mathrm{s}}$ |
| Internal Power Dissipation | 250 mW |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering 10 sec$)$ | $300^{\circ} \mathrm{C}$ |

${ }^{1}$ Thermal resistance measured on SEMI standard 4-layer board. 8 -lead SOIC: $\theta_{J A}=121^{\circ} \mathrm{C} / \mathrm{W}$.
8 -lead MSOP: $\theta_{J A}=142^{\circ} \mathrm{C} / \mathrm{W}$.

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only, functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.


Figure 3. Plot of Maximum Power Dissipation vs. Temperature

## ESD CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.


## AD8131

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



Figure 4. Pin Configuration

Table 6. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 1 | -Din | Negative Input. |
| 2 | Vocm | Common-Mode Output Voltage. Voltage applied to this pin sets the common-mode output voltage with a ratio of 1:1. For example, 1 V dc on Vосм will set the dc bias level on +OUT and -OUT to 1 V . |
| 3 | V+ | Positive Supply Voltage. |
| 4 | +OUT | Positive Output. Note: the voltage at - $\mathrm{DIN}_{\text {IN }}$ is inverted at + OUT. |
| 5 | -OUT | Negative Output. Note: the voltage at $+\mathrm{D}_{\mathrm{IN}}$ is inverted at -OUT. |
| 6 | V- | Negative Supply Voltage. |
| 7 | NC | No Connect. |
| 8 | $+\mathrm{D}_{\text {IN }}$ | Positive Input. |

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 5. Basic Test Circuit


Figure 6. Small Signal Frequency Response


Figure 7. Small Signal Frequency Response


Figure 8. Large Signal Frequency Response


Figure 9. Large Signal Frequency Response


Figure 10. Harmonic Distortion Test Circuit $\left(R_{L, d m}=800 \Omega\right)$

## AD8131



Figure 11. Harmonic Distortion vs. Frequency


Figure 12. Harmonic Distortion vs. Frequency


Figure 13. Harmonic Distortion vs. Differential Output Voltage


Figure 14. Harmonic Distortion vs. Differential Output Voltage


Figure 15. Harmonic Distortion vs. Differential Output Voltage


Figure 16. Harmonic Distortion vs. R LOAD


Figure 17. Harmonic Distortion vs. R LOAD


Figure 18. Harmonic Distortion vs. RLOAD


Figure 19. Intermodulation Distortion


Figure 20. Third Order Intercept vs. Frequency


Figure 21. Large Signal Transient Response


Figure 22. Small Signal Transient Response

## AD8131



Figure 23. Large Signal Transient Response


Figure 24. Large Signal Transient Response


Figure 25. 0.1\% Settling Time


Figure 26. Capacitor Load Drive Test Circuit


Figure 27. Large Signal Transient Response for Various Capacitor Loads


Figure 28. PSRR vs. Frequency


Figure 29. CMRR Test Circuit


Figure 30. CMRR vs. Frequency


Figure 31. Single-Ended $Z_{\text {OUt }}$ vs. Frequency


Figure 32. Output Balance Error Test Circuit


Figure 33. Output Balance Error vs. Frequency


Figure 34. Quiescent Current vs. Temperature


Figure 35. Voltage Noise vs. Frequency


Figure 36. V осм Gain Response


Figure 37. Vосм CMRR vs. Frequency


Figure 38. Vосм Transient Response

## AD8131

## OPERATIONAL DESCRIPTION



Figure 39. Circuit Definitions
Differential voltage refers to the difference between two node voltages. For example, the output differential voltage (or equivalently output differential-mode voltage) shown in Figure 39 is defined as

$$
V_{\text {OUT }, d m}=\left(V_{+O U T}-V_{- \text {OUT }}\right)
$$

$\mathrm{V}_{\text {+out }}$ and $\mathrm{V}_{\text {-out }}$ refer to the voltages at the +OUT and -OUT terminals with respect to a common reference.

Common-mode voltage refers to the average of two node voltages. The output common-mode voltage is defined as

$$
V_{\text {OUT }, c m}=\left(V_{+O U T}+V_{-O U T}\right) / 2
$$

Balance is a measure of how well differential signals are matched in amplitude and exactly 180 degrees apart in phase. Balance is most easily determined by placing a well-matched resistor divider between the differential voltage nodes and comparing the magnitude of the signal at the divider's midpoint with the magnitude of the differential signal. By this definition, output balance is the magnitude of the output common-mode voltage divided by the magnitude of the output differentialmode voltage.

$$
\text { Output Balance Error }=\left|\frac{V_{\text {OUT, cm }}}{V_{\text {OUT, dm }}}\right|
$$

## THEORY OF OPERATION

The AD8131 differs from conventional op amps in that it has two outputs whose voltages move in opposite directions. Like an op amp, it relies on high open-loop gain and negative feedback to force these outputs to the desired voltages. The AD8131 behaves much like a standard voltage feedback op amp and makes it easy to perform single-ended-to-differential conversion, common-mode level-shifting, and amplification of differential signals.

Previous discrete and integrated differential driver designs used two independent amplifiers and two independent feedback loops, one to control each of the outputs. When these circuits are driven from a single-ended source, the resulting outputs are typically not well balanced. Achieving a balanced output typically required exceptional matching of the amplifiers and feedback networks.

DC common-mode level shifting has also been difficult with previous differential drivers. Level shifting required the use of a third amplifier and feedback loop to control the output common-mode level. Sometimes the third amplifier has also been used to attempt to correct an inherently unbalanced circuit. Excellent performance over a wide frequency range has proven difficult with this approach.

The AD8131 uses two feedback loops to separately control the differential and common-mode output voltages. The differential feedback, set by internal resistors, controls only the differential output voltage. The common-mode feedback controls only the common-mode output voltage. This architecture makes it easy to arbitrarily set the common-mode output level. It is forced, by internal common-mode feedback, to be equal to the voltage applied to the Vосм input, without affecting the differential output voltage.

The AD8131 architecture results in outputs that are very highly balanced over a wide frequency range without requiring external components or adjustments. The common-mode feedback loop forces the signal component of the output common-mode voltage to be zeroed. The result is nearly perfectly balanced differential outputs, of identical amplitude and exactly 180 degrees apart in phase.

## ANALYZING AN APPLICATION CIRCUIT

The AD8131 uses high open-loop gain and negative feedback to force its differential and common-mode output voltages in such a way as to minimize the differential and common-mode error voltages. The differential error voltage is defined as the voltage between the differential inputs labeled +IN and -IN in Figure 39. For most purposes, this voltage can be assumed to be zero. Similarly, the difference between the actual output common-mode voltage and the voltage applied to Vосм can also
be assumed to be zero. Starting from these two assumptions, any application circuit can be analyzed.

## CLOSED-LOOP GAIN

The differential mode gain of the circuit in Figure 39 can be described by the following equation:

$$
\left|\frac{V_{\text {OUT, } d m}}{V_{I N, d m}}\right|=\frac{R_{F}}{R_{G}}=2
$$

where $R_{F}=1.5 \mathrm{k} \Omega$ and $R_{G}=750 \Omega$ nominally.

## ESTIMATING THE OUTPUT NOISE VOLTAGE

Similar to the case of a conventional op amp, the differential output errors (noise and offset voltages) can be estimated by multiplying the input referred terms, at +IN and -IN , by the circuit noise gain. The noise gain is defined as

$$
G_{N}=1+\left(\frac{R_{F}}{R_{G}}\right)=3
$$

The total output referred noise for the AD8131, including the contributions of $\mathrm{R}_{\mathrm{F}}, \mathrm{R}_{\mathrm{G}}$, and op amp, is nominally $25 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$ at 20 MHz .

## CALCULATING THE INPUT IMPEDANCE OF AN APPLICATION CIRCUIT

The effective input impedance of a circuit such as that in Figure 39 , at $+D_{\text {IN }}$ and $-D_{\text {IN }}$, will depend on whether the amplifier is being driven by a single-ended or differential signal source. For balanced differential input signals, the input impedance ( $R_{I N, d m}$ ) between the inputs ( $+\mathrm{D}_{\text {IN }}$ and $-\mathrm{D}_{\text {IN }}$ ) is

$$
R_{I N, d m}=2 \times R_{G}=1.5 \mathrm{k} \Omega
$$

In the case of a single-ended input signal (for example if $-\mathrm{D}_{\mathrm{IN}}$ is grounded and the input signal is applied to $+\mathrm{D}_{\text {IN }}$ ), the input impedance becomes

$$
R_{I N, d m}=\left(\frac{R_{G}}{1-\frac{R_{F}}{2 \times\left(R_{G}+R_{F}\right)}}\right)=1.125 \mathrm{k} \Omega
$$

The input impedance is effectively higher than it would be for a conventional op amp connected as an inverter because a fraction of the differential output voltage appears at the inputs as a common-mode signal, partially bootstrapping the voltage across the input resistor $\mathrm{R}_{\mathrm{G}}$.

## INPUT COMMON-MODE VOLTAGE RANGE IN SINGLE-SUPPLY APPLICATIONS

The AD8131 is optimized for level-shifting ground referenced input signals. For a single-ended input this would imply, for example, that the voltage at $-\mathrm{D}_{\text {IN }}$ in Figure 39 would be zero volts when the amplifier's negative power supply voltage (at $\mathrm{V}-$ ) was also set to zero volts.

## SETTING THE OUTPUT COMMON-MODE VOLTAGE

The AD8131's Voсм pin is internally biased at a voltage approximately equal to the midsupply point (average value of the voltages on $\mathrm{V}+$ and $\mathrm{V}-$ ). Relying on this internal bias results in an output common-mode voltage that is within about 25 mV of the expected value.

In cases where more accurate control of the output commonmode level is required, it is recommended that an external source, or resistor divider (made up of $10 \mathrm{k} \Omega$ resistors), be used.

## DRIVING A CAPACITIVE LOAD

A purely capacitive load can react with the pin and bondwire inductance of the AD8131 resulting in high frequency ringing in the pulse response. One way to minimize this effect is to place a small resistor in series with the amplifier's outputs as shown in Figure 26.

## APPLICATIONS

## TWISTED-PAIR LINE DRIVER

The AD8131 has on-chip resistors that provide for a gain of 2 without any external parts. Several on-chip resistors are trimmed to ensure that the gain is accurate, the common-mode rejection is good, and the output is well balanced. This makes the AD8131 very suitable as a single-ended-to-differential twisted-pair line driver.

Figure 40 shows a circuit of an AD8131 driving a twisted-pair line, like a Category 3 or Category 5 (Cat 3 or Cat5), that is already installed in many buildings for telephony and data communications. The characteristic impedance of such a transmission line is usually about $100 \Omega$. The outstanding balance of the AD8131 output will minimize the commonmode signal and therefore the amount of EMI generated by driving the twisted pair.

The two resistors in series with each output terminate the line at the transmit end. Since the impedances of the outputs of the AD8131 are very low, they can be thought of as a short-circuit, and the two terminating resistors form a $100 \Omega$ termination at the transmit end of the transmission line. The receive end is directly terminated by a $100 \Omega$ resistor across the line.

This back-termination of the transmission line divides the output signal by two. The fixed gain of 2 of the AD8131 will create a net unity gain for the system from end to end.

In this case, the input signal is provided by a signal generator with an output impedance of $50 \Omega$. This is terminated with a $49.9 \Omega$ resistor near $+\mathrm{D}_{\text {IN }}$ of the AD8131. The effective parallel resistance of the source and termination is $25 \Omega$.The $24.9 \Omega$ resistor from $-D_{\text {IN }}$ to ground matches the $+\mathrm{D}_{\text {IN }}$ source impedance and minimizes any dc and gain errors.

If $+\mathrm{D}_{\text {IN }}$ is driven by a low-impedance source over a short distance, such as the output of an op amp, then no termination resistor is required at $+\mathrm{D}_{\text {IN }}$. In this case, the $-\mathrm{D}_{\text {IN }}$ can be directly tied to ground.


## 3 V SUPPLY DIFFERENTIAL A-TO-D DRIVER

Many newer ADCs can run from a single 3 V supply, which can save significant system power. In order to increase the dynamic range at the analog input, they have differential inputs, which double the dynamic range with respect to a single-ended input. An added benefit of using a differential input is that the distortion can be improved.

The low distortion and ability to run from a single 3 V supply make the AD8131 suited as an A-to-D driver for some 10-bit, singlesupply applications. Figure 41 shows a schematic for a circuit for an AD8131 driving an AD9203, a 10-bit, 40 MSPS ADC.

The common mode of the AD8131 output is set at midsupply by the voltage divider connected to Vосм, and ac-bypassed with a $0.1 \mu \mathrm{~F}$ capacitor. This provides for maximum dynamic range between the supplies at the output of the AD8131. The $110 \Omega$ resistors at the AD8131 output, along with the shunt capacitors form a one pole, low-pass filter for lowering noise and antialiasing.


Figure 41. Test Circuit for AD8131 Driving an AD9203, 10-Bit, 40 MSPS ADC
Figure 42 shows an FFT plot that was taken from the combined devices at an analog input frequency of 2.5 MHz and a 40 MSPS sampling rate. The performance of the AD8131 compares very favorably with a center-tapped transformer drive, which has typically been the best way to drive this ADC. The AD8131 has the advantage of maintaining dc performance, which a transformer solution cannot provide.

Figure 40. Single-Ended-to-Differential $100 \Omega$ Line Driver


Figure 42. FFT Plot for AD8131/AD9203

## UNITY-GAIN, SINGLE-ENDED-TO-DIFFERENTIAL DRIVER

If it is not necessary to offset the output common-mode voltage (via the Vосм pin ), then the AD8131 can make a simple unitygain single-ended-to-differential amplifier that does not require any external components. Figure 43 shows the schematic for this circuit.


Figure 43. Unity Gain, Single-Ended-to-Differential Amplifier

As shown above, when $-D_{\text {IN }}$ is left floating, there is $100 \%$ feedback of +OUT to -IN via the internal feedback resistor. This contrasts with the typical gain of 2 operation where $-D_{\text {IN }}$ is grounded and one third of the +OUT is fed back to -IN. The result is a closed-loop differential gain of 1 .

Upon careful observation, it can be seen that only $+D_{\text {IN }}$ and $V_{\text {OCM }}$ are referenced to ground. The ground voltage at $\mathrm{V}_{\text {осм }}$ is the reference for this circuit. In this unity gain configuration, if a dc voltage is applied to V differential dc voltage will be created at the output, along with the common-mode voltage change. Thus, this configuration cannot be used when it is desired to offset the common-mode voltage of the output with respect to the input at $+\mathrm{D}_{\text {IN }}$.

## AD8131

## OUTLINE DIMENSIONS



Figure 44. 8-Lead Standard Small Outline Package [SOIC_N] Narrow Body
( $R-8$ )
Dimensions shown in millimeters and (inches)


COPLANARITY SEATING
0.10 PLANE

COMPLIANT TO JEDEC STANDARDS MO-187-AA
Figure 45. 8-Lead Mini Small Outline Package [MSOP]
(RM-8)
Dimensions shown in millimeters

## ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Option | Branding |
| :---: | :---: | :---: | :---: | :---: |
| AD8131AR | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| AD8131AR-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC, 13" Tape and Reel | R-8 |  |
| AD8131AR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC, 7" Tape and Reel | R-8 |  |
| AD8131ARZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| AD8131ARZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC, 13" Tape and Reel | R-8 |  |
| AD8131ARZ-REEL7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC, 7" Tape and Reel | R-8 |  |
| AD8131ARM | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Mini Small Outline Package [MSOP] | RM-8 | HJA |
| AD8131ARM-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP, 13" Tape and Reel | RM-8 | HJA |
| AD8131ARM-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP, 7" Tape and Reel | RM-8 | HJA |
| AD8131ARMZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Mini Small Outline Package [MSOP] | RM-8 | HJA\# |
| AD8131ARMZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP, 13" Tape and Reel | RM-8 | HJA\# |
| AD8131ARMZ-REEL7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP, 7" Tape and Reel | RM-8 | HJA\# |

${ }^{1} \mathrm{Z}=$ Pb-free part, \# denotes Pb-free part; may be top or bottom marked.
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